

15/7/2021  
L6 online

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**ENEE2360**  
**Analog Electronics**

**T4:**  
**Diode Applications**

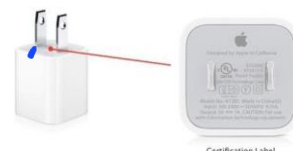
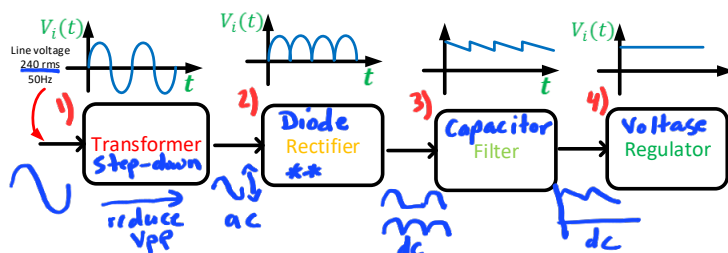
**Instructor: Nasser Ismail**

# Dc Power Supply

- All electronic circuits and systems require a stable source of dc voltage and current ( or dc power) to operate correctly.

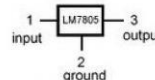
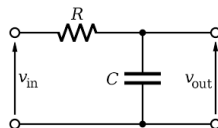
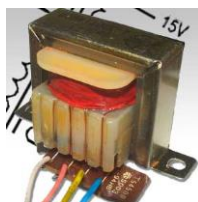


Lab

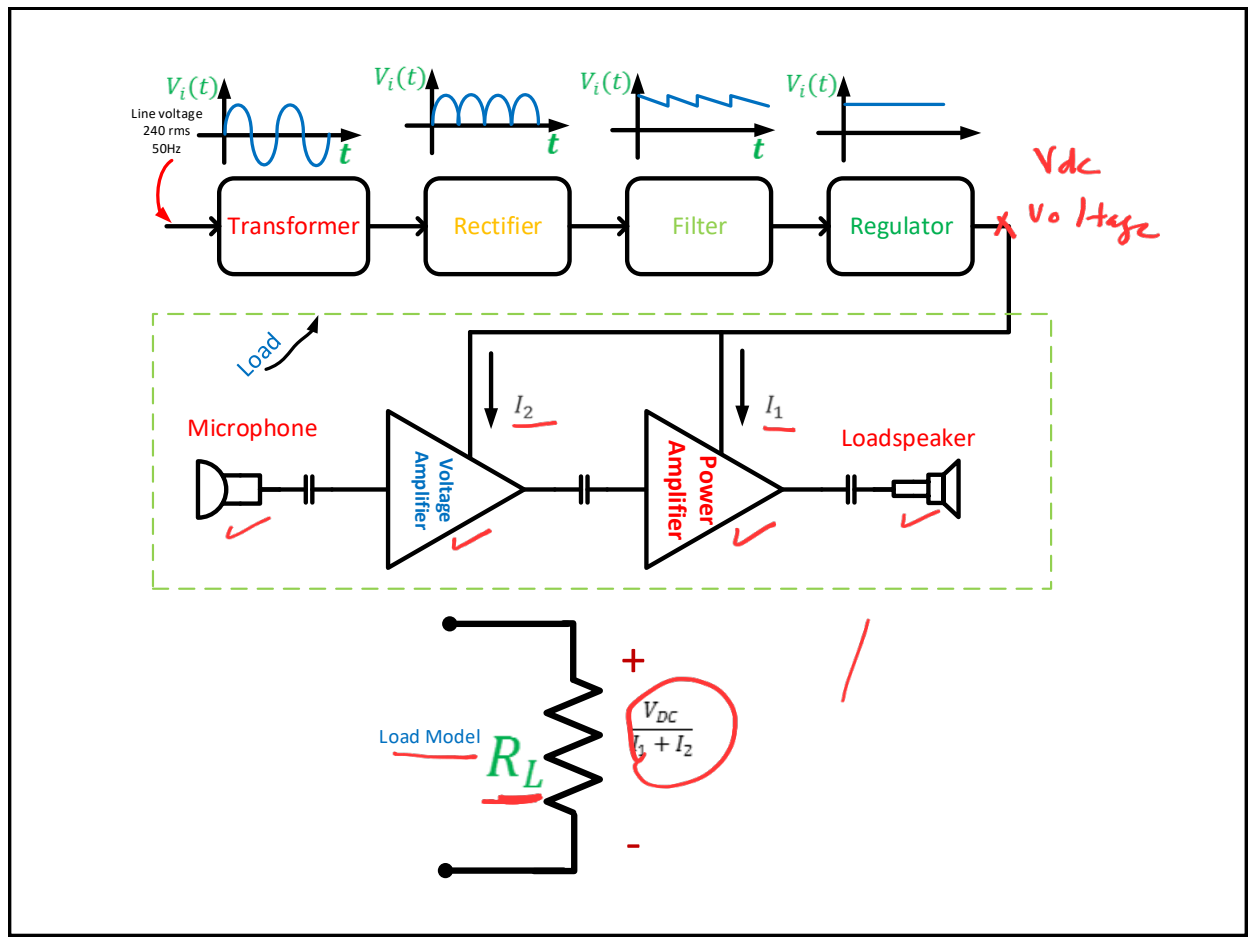
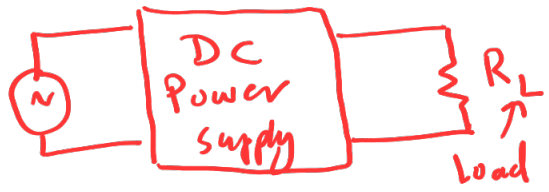


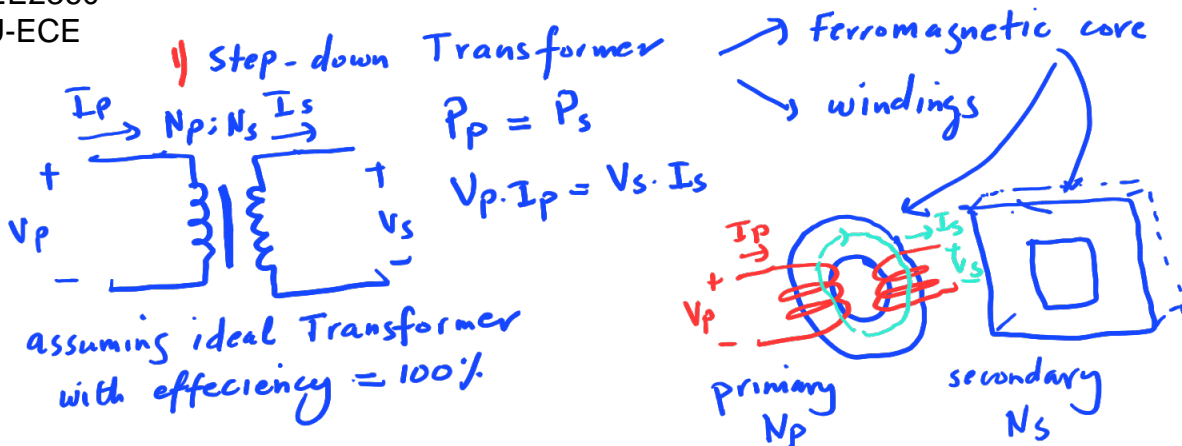
Apple 5W USB Charger (Credit: Apple)

chargers



Block diagram of a dc power supply.

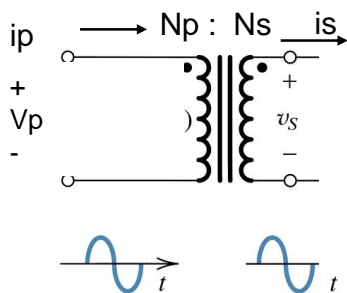




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## Designing a power supply

1) Transformer → used for ac voltages \*\*



$$\frac{V_p}{V_s} = \frac{N_p}{N_s}$$

$$\frac{I_p}{I_s} = \frac{N_s}{N_p} = n$$

Usually steps down type to decrease the amplitude of the ac line voltage

$$\frac{V_p}{V_s} = \frac{N_p}{N_s} \quad \checkmark$$

$$\frac{i_s}{i_p} = \frac{N_p}{N_s} \quad \checkmark$$

$$\frac{V_s}{V_p} = \frac{N_s}{N_p} = n$$

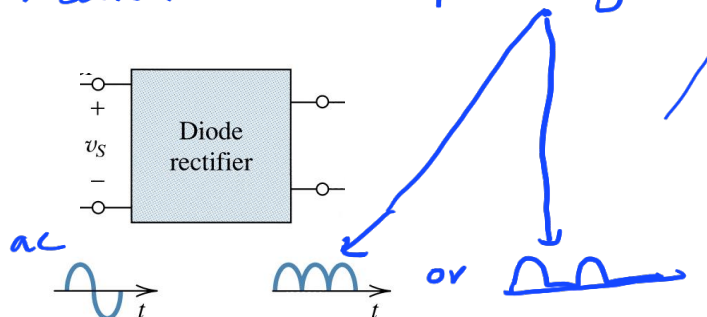
$$n = \frac{N_s}{N_p} \quad \text{transformer turns ratio}$$

$$\Rightarrow V_s = nV_p$$



## Designing a power supply

2) Rectifier : *converts ac to pulsating dc*



➤ Used to convert ac voltage (with zero average value) to pulsating dc voltage (non zero average)

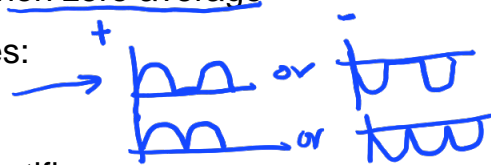
➤ Rectifiers are two types:

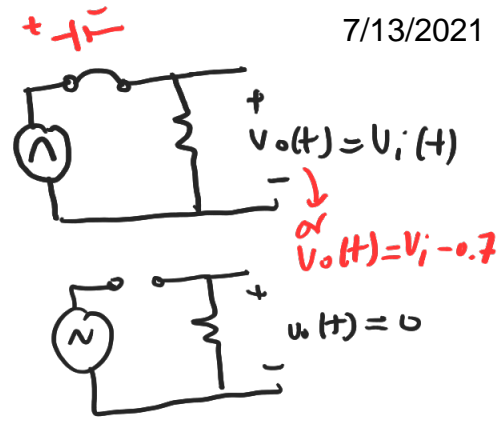
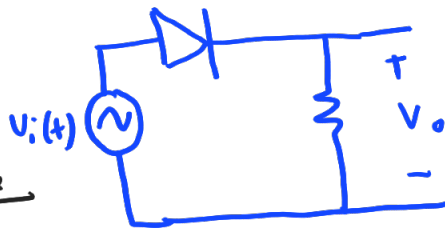
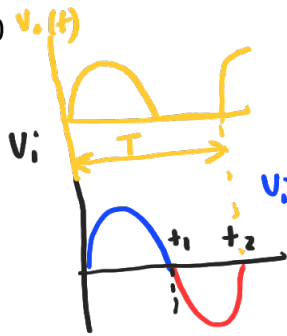
a) Half Wave Rectifier

b) Full Wave Rectifier

✓ - Bridge Full Wave Rectifier

✓ - Center Tapped Transformer Full Wave Rectifier



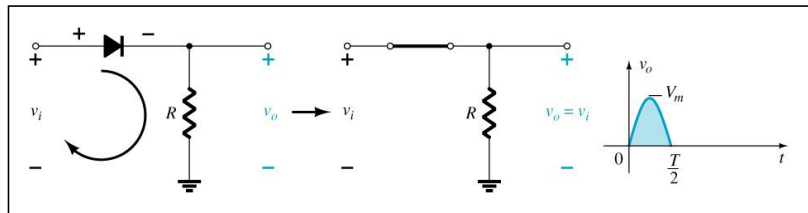


1) if  $v_i(t) > 0 \rightarrow$  Diode is ON  $\rightarrow$   
 2) " "  $< 0 \rightarrow$  " " off  $\rightarrow$

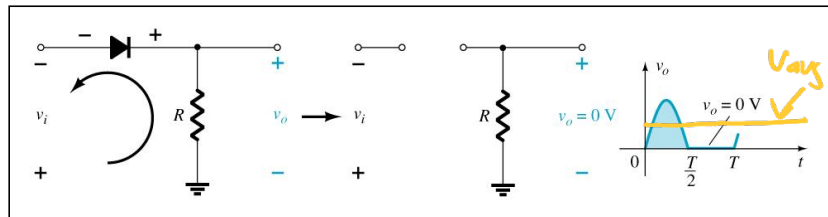
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# Half Wave Rectifier

1) When  $V_i(t) > 0$ ,  
 Diode is ON  
 $V_o = V_i$



2) When  $V_i(t) < 0$ ,  
 Diode is OFF  
 $V_o = 0$



The diode conducts only when it is forward biased, therefore only half of the AC cycle passes through the diode to the output.

$$V_{AVG} = \frac{1}{T} \int_0^T V_m \sin(\omega t) dt \quad \leftarrow \text{by definition } V_{avg} \equiv V_{dc} \equiv V_{mean}$$

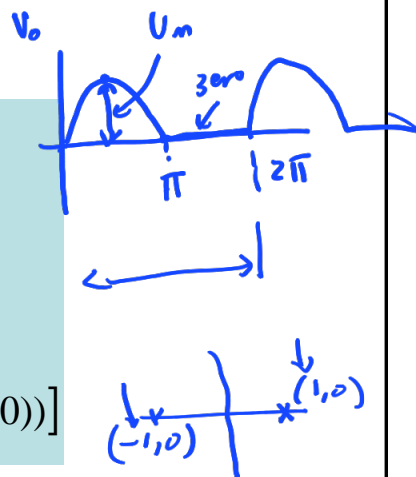
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# Half Wave Rectifier

$$V_{AVG} = \frac{1}{T} \int_0^T V_m \sin(\omega t) dt$$

$$= \frac{1}{2\pi} \int_0^\pi V_m \sin(\theta) d\theta$$

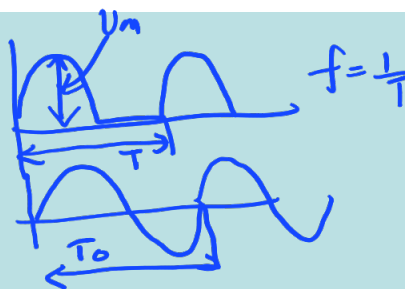
$$= \frac{1}{2\pi} [-V_m \cos(\theta)]_0^\pi = \frac{V_m}{2\pi} [-\cos(\pi) - (-\cos(0))]$$



$$V_{AVG} = \frac{V_m}{2\pi} [ -(-1) - (-1) ]$$

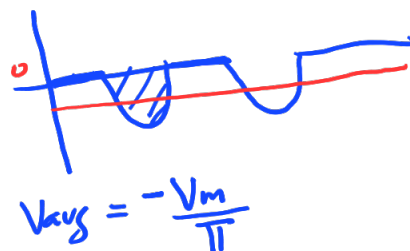
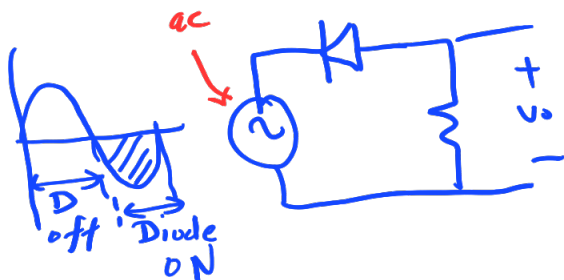
$$= \frac{2V_m}{2\pi} = \frac{V_m}{\pi} \approx 0.318V_m$$

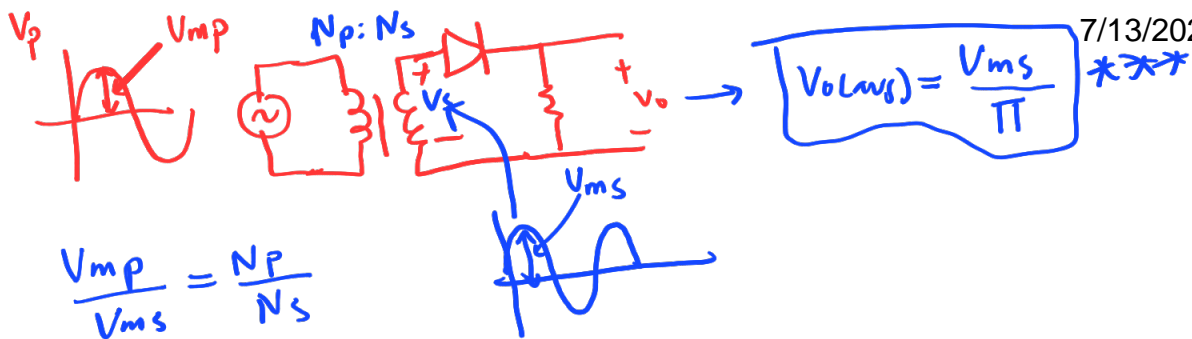
to remember



$T = T_o$  and  $f = f_o$

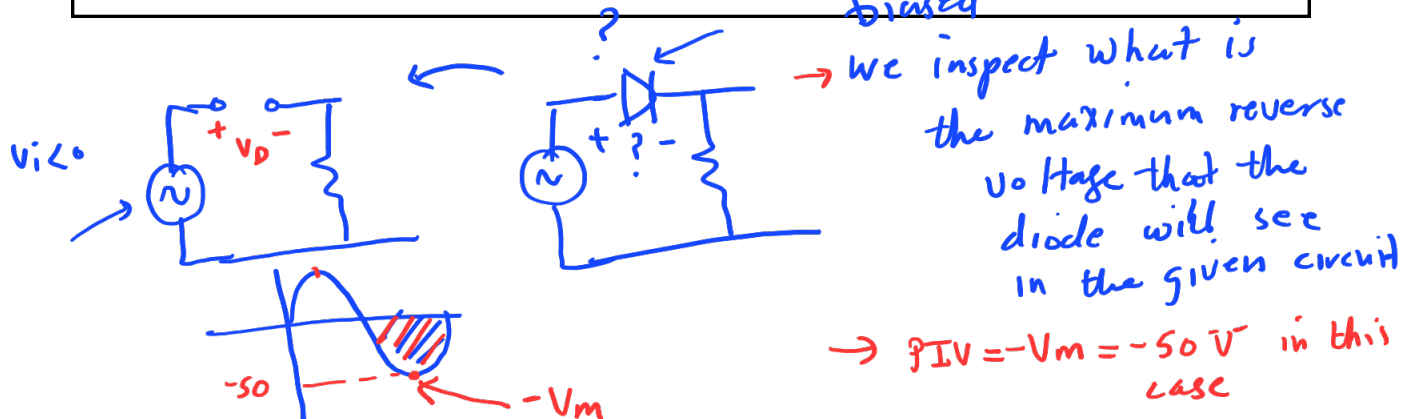
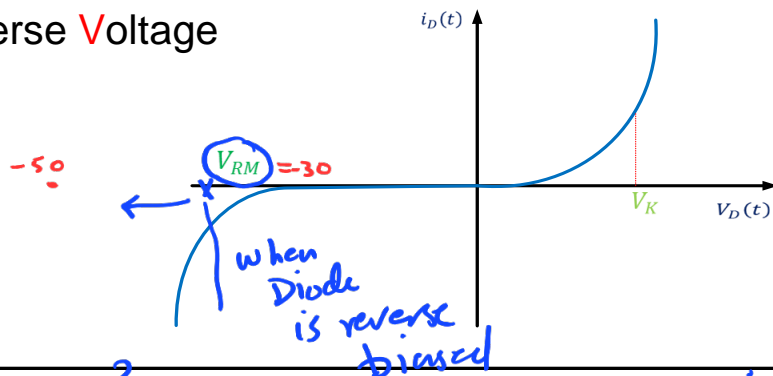
(period and frequency of the rectified waveform is the same as ac input)





## X Important Electrical Ratings *later*

- $I_{FM}$  = maximum forward current
- $I_{FM}$  = maximum average current that can safely be sustained by the diode when it is forward biased
- $V_{RM}$  = maximum reverse voltage
- $V_{RM}$  = maximum voltage that can be applied to the diode in the reverse bias polarity before voltage break down occur
- PIV  $\equiv$  Peak Inverse Voltage
- $PIV = V_{RM}$



## PIV (For Half Wave Rectifier)

Because the diode is only forward biased for one-half of the AC cycle, it is also reverse biased for one-half cycle.

It is important that the reverse breakdown voltage rating of the diode be high enough to withstand the peak, reverse-biasing AC voltage.

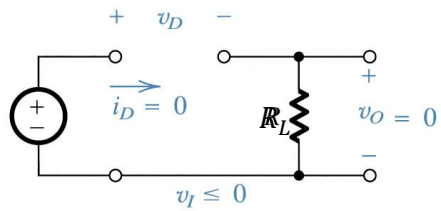
$$V_D(t) = V_i(t)$$

$$V_{D(t)\max} = -V_m$$

$$\text{PIV} = -V_m$$

$$I_{FM} = \frac{V_{AVG}}{R_L} = I_{RL}$$

$$I_{FM} = \frac{V_m}{\pi R_L}$$



# Full-Wave Rectification

T

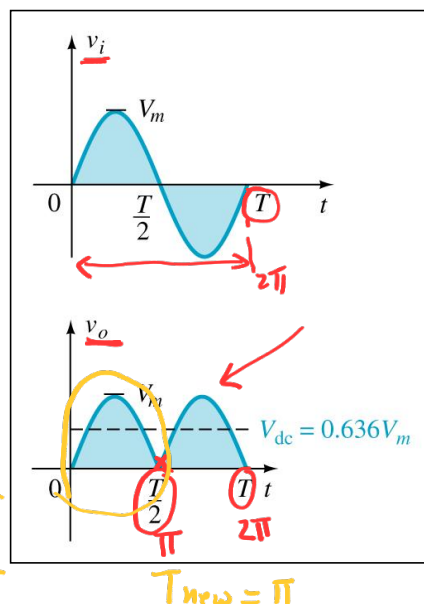
The rectification process can be improved by using a full-wave rectifier circuit.

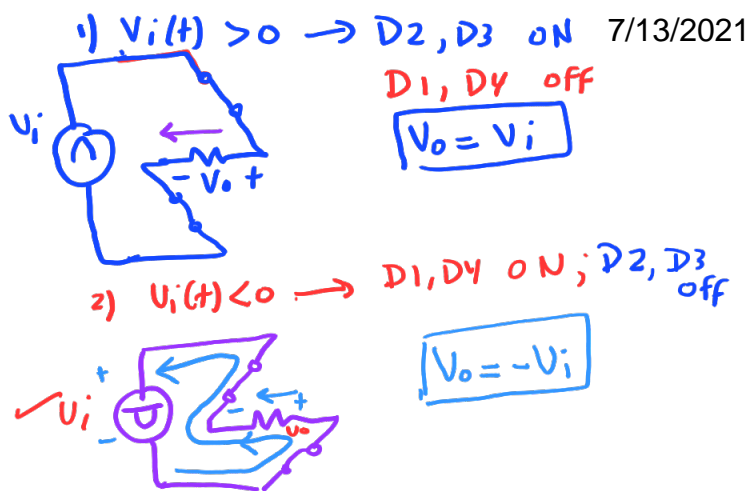
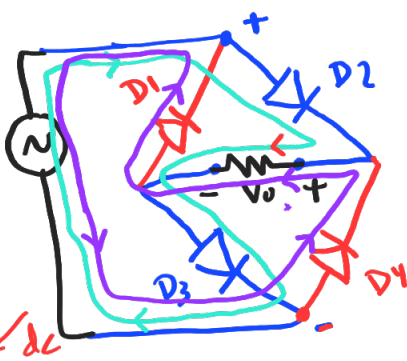
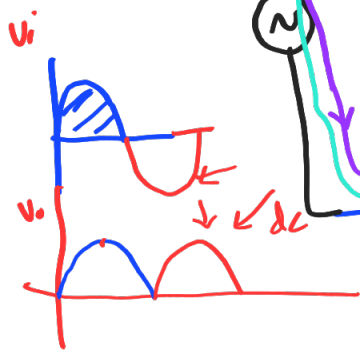
Full-wave rectification produces a greater DC output:

$$V_{avg} = \frac{1}{T} \int_0^T f(t) dt = \frac{1}{\pi} \int_0^{\pi} f(t) dt$$

Half-wave:  $V_{dc} = 0.318 V_m = \frac{V_m}{\pi}$

Full-wave:  $V_{dc} = 0.636 V_m = \frac{2V_m}{\pi}$





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# Bridge Full-Wave Rectifier

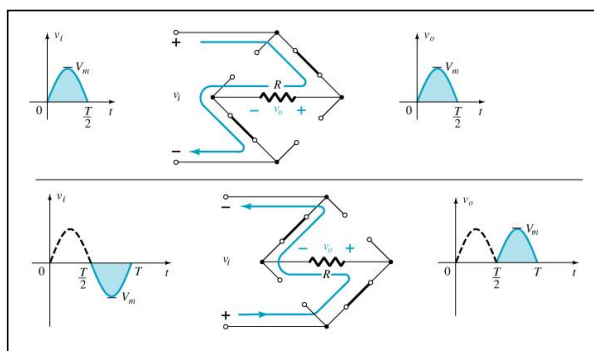
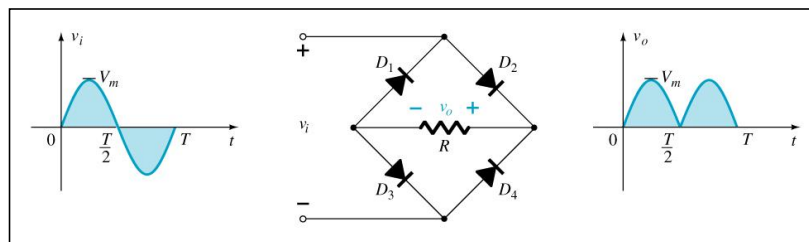
A full-wave rectifier with four diodes that are connected in a bridge configuration

1) When  $V_i(t) > 0$ ,  
D2, D3 are ON  
D1, D4 are OFF

$\Rightarrow V_o(t) = V_i(t)$

2) When  $V_i(t) < 0$ ,  
D2, D3 are OFF  
D1, D4 are ON

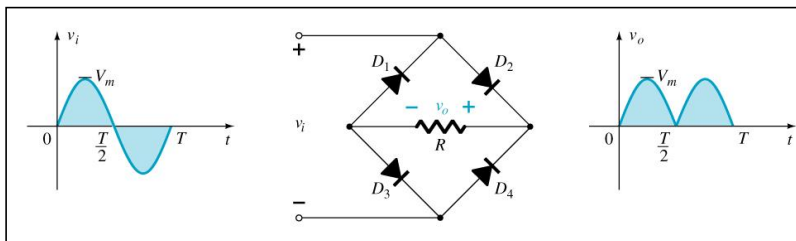
$\Rightarrow V_o(t) = -V_i(t)$



## Bridge Full-Wave Rectifier

$$V_{AVG} = \frac{1}{T} \int_0^T V_m \sin(\omega t) dt$$

$$= \frac{1}{\pi} \int_0^{\pi} V_m \sin(\theta) d\theta$$



$$V_{AVG} = \frac{2V_m}{\pi} \cong 0.636V_m$$

$$T = \frac{T_o}{2} \text{ and } f = 2f_o$$

(period and frequency of the rectified waveform is not the same as ac input)



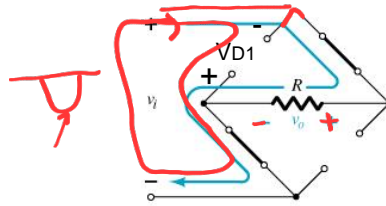
# PIV for each of the 4 diodes

For ideal diode

$$V_{D1}(t) = -V_i(t)$$

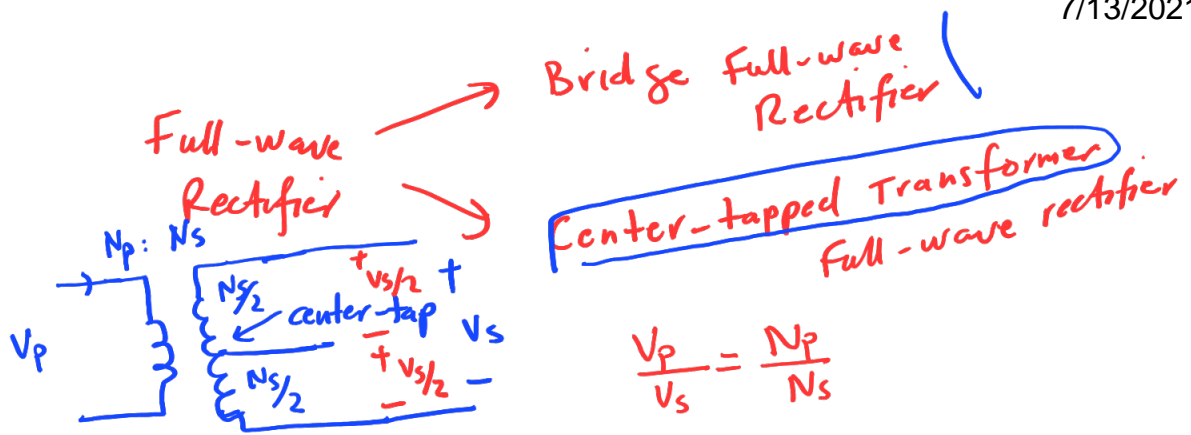
$$V_{D1}(t)_{\max} = -V_m$$

$$\text{PIV} = -V_m$$



$$V_i + V_{D1} = 0$$

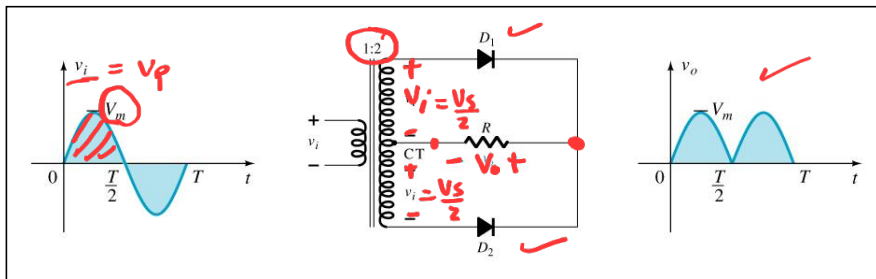
$$V_{D1} = -V_i$$



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## Center Tapped Transformer Full-Wave Rectifier

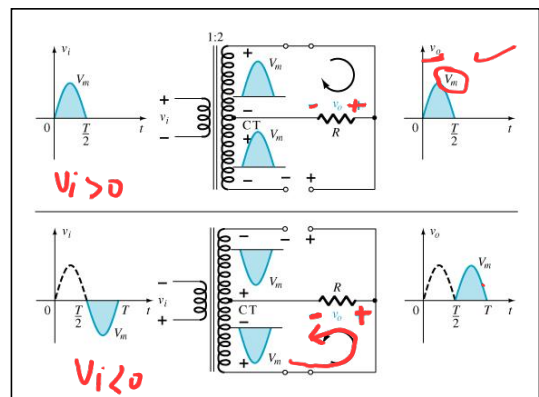
Special case



$N_p = 1$   
 $N_s = 2$   
 $\frac{V_p}{V_s} = \frac{1}{2}$   
 $V_s = 2 V_p$   
 $\frac{V_s}{2} = V_p$

Requires two diodes and a center-tapped transformer

**Note:** *صلاطظ هامة جدا*  
 if turns ratio is other than 1:2, make sure to calculate  $V_m$  at the secondary side correctly



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# CT Transformer Full-Wave Rectifier

1) When  $V_i(t) > 0$ ,

D1 is ON

D2 is OFF

$$\Rightarrow V_o(t) = V_i(t)$$

2) When  $V_i(t) < 0$ ,

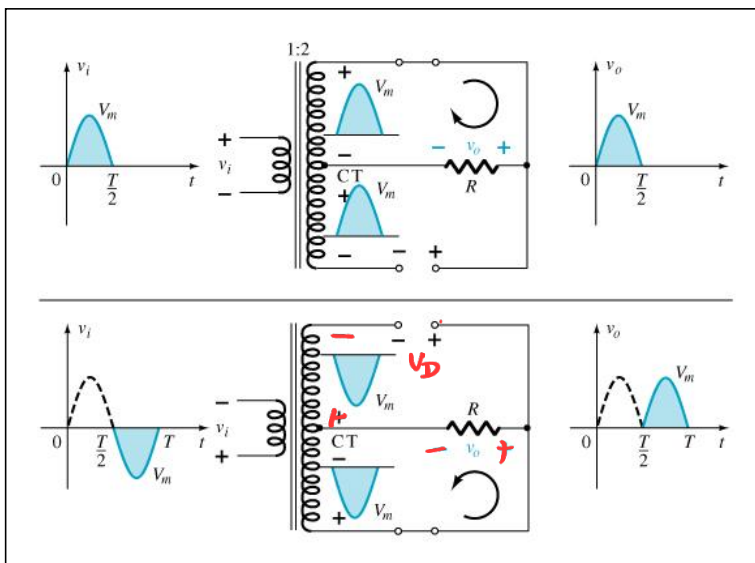
D1 is OFF

D2 is ON

$$\Rightarrow V_o(t) = -V_i(t)$$

$$V_{AVG} = \frac{2V_m}{\pi} \cong 0.636V_m$$

$$T = \frac{T_o}{2} \text{ and } f = 2f_o$$

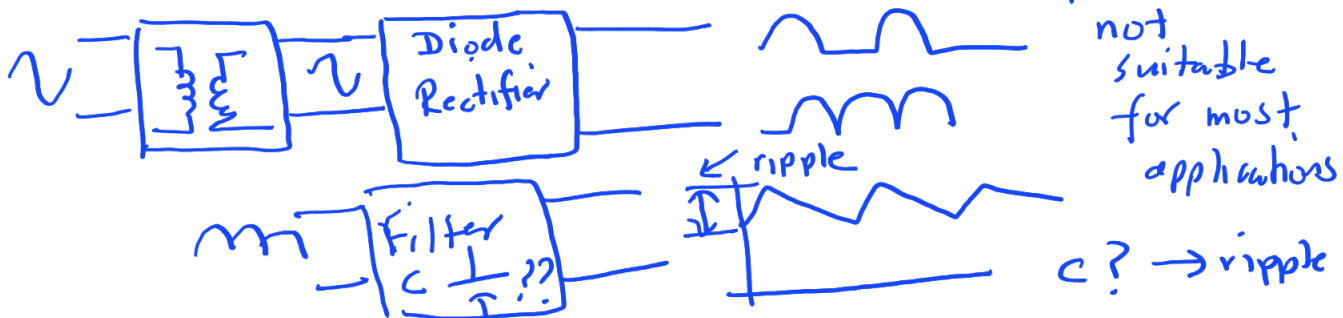


$\nearrow PIV = -2V_m$

	Half wave	Bridge	center-tapped
Diodes	1	(4)	(2)
Transformer	regular	regular	center-tapped
avg-voltage	$0.318 V_m$	$0.636 V_m$	$0.636 V_m$
PIV	$-V_m$	$-V_m$	$-2V_m$

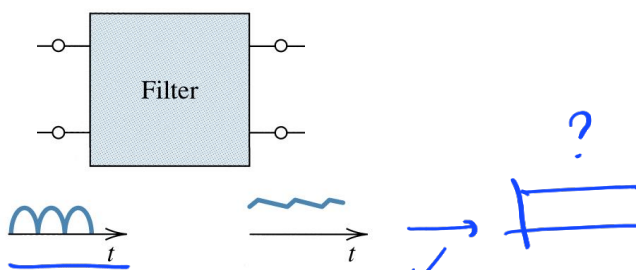
End of L6

dc Power supply

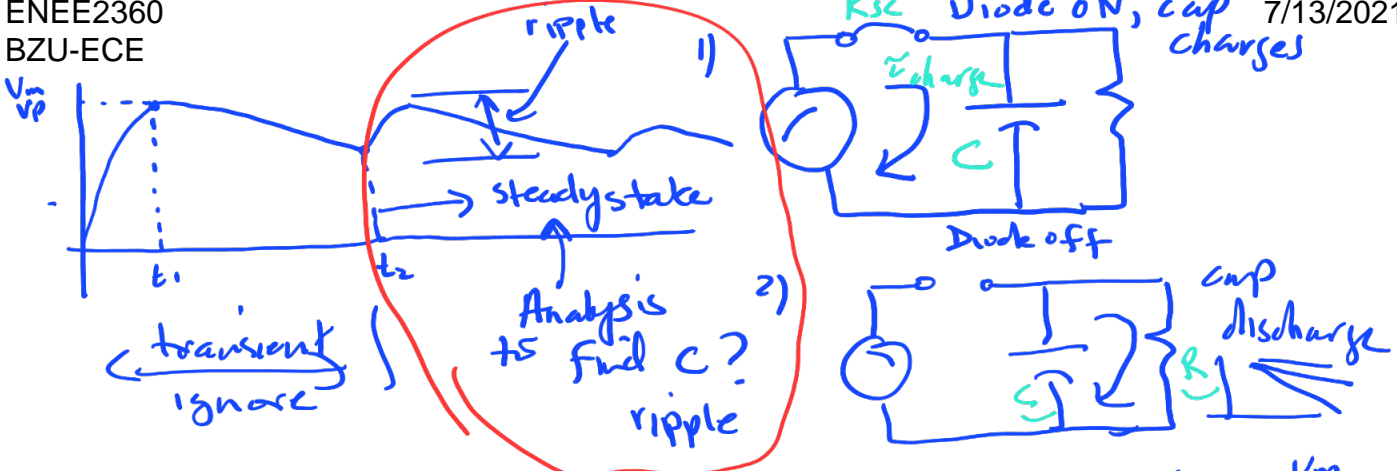


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3) Filter

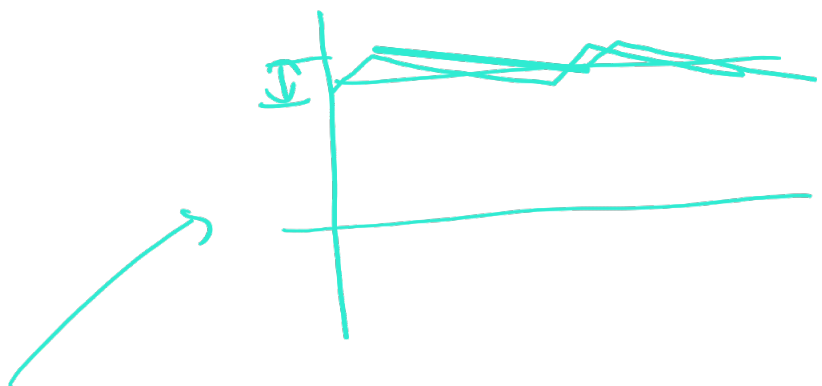
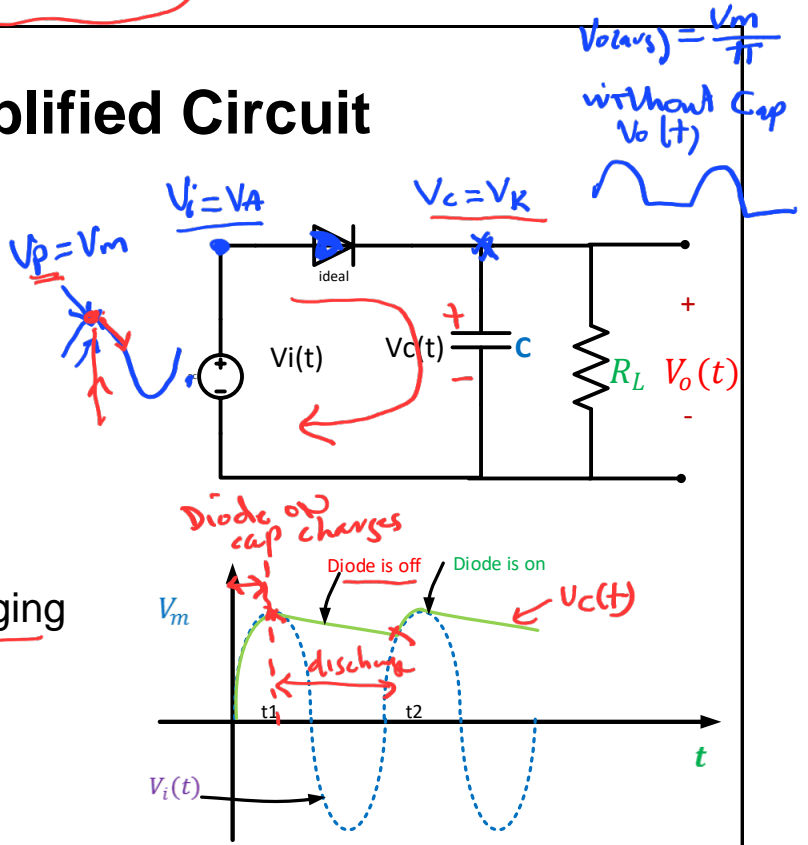


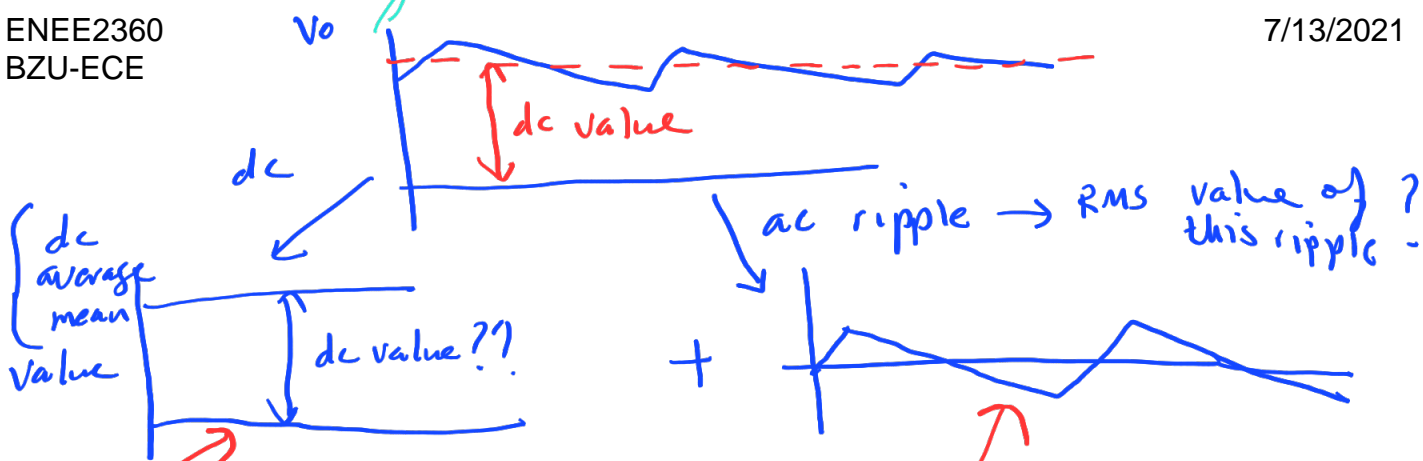
- One of dc power supply components
- Used to smooth out (remove) the pulsating DC produced by the rectifiers and to pass only the DC component (average value; mean value)



## Simplified Circuit

- A) when  $V_i(t) > V_c(t)$  ;  
Diode is on and  $V_o(t) = V_c(t) = V_i(t)$
- B) when  $V_i(t) < V_c(t)$  ;  
Diode is off and the capacitor starts discharging

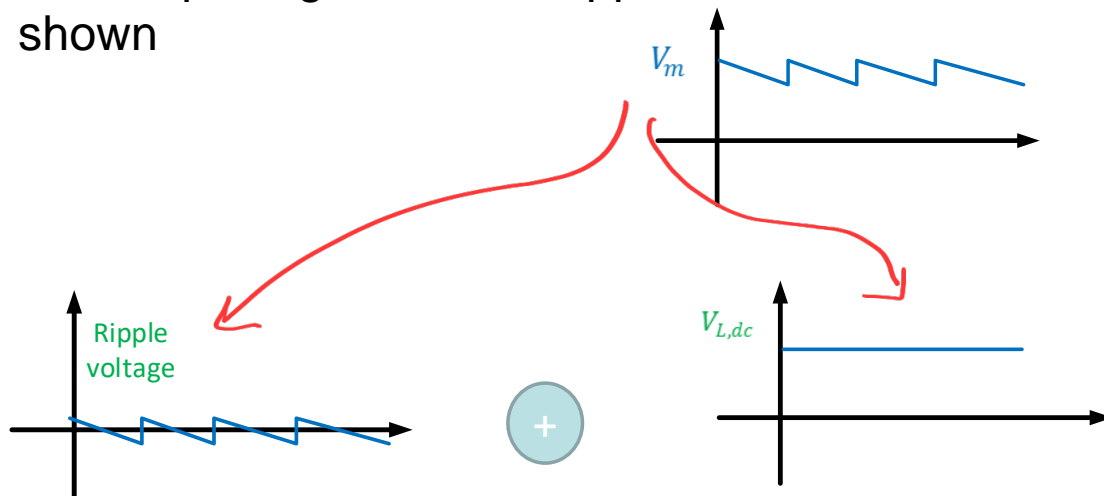




- Ripple factor is an indicator for the effectiveness of the filter

$$r\% = \frac{\text{RMS(ripple of output voltage)}}{\text{Average value of the output signal}} \times 100\%$$

- The output signal can be approximated as shown

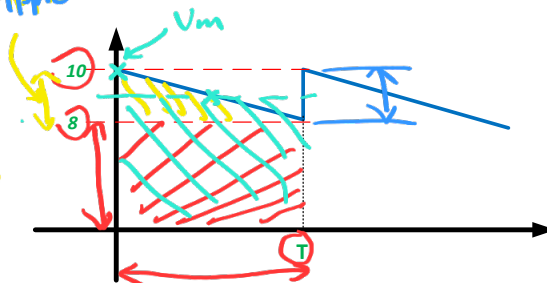


### Example

Find average output voltage?

$$V_{dc} = V_{avg} = \frac{1}{T} \int_0^T f(t) dt$$

peak to peak } →  $V_{Lr, PP}$   
ripple →



$$\begin{aligned} V_{O,DC} &= V_{O,AVG} = \frac{1}{T} \int_0^T V_O(t) dt \\ &= \frac{1}{T} (\text{Area}) \\ &= \frac{1}{T} \left( 8T + \frac{2T}{2} \right) = \underline{9V} \end{aligned}$$

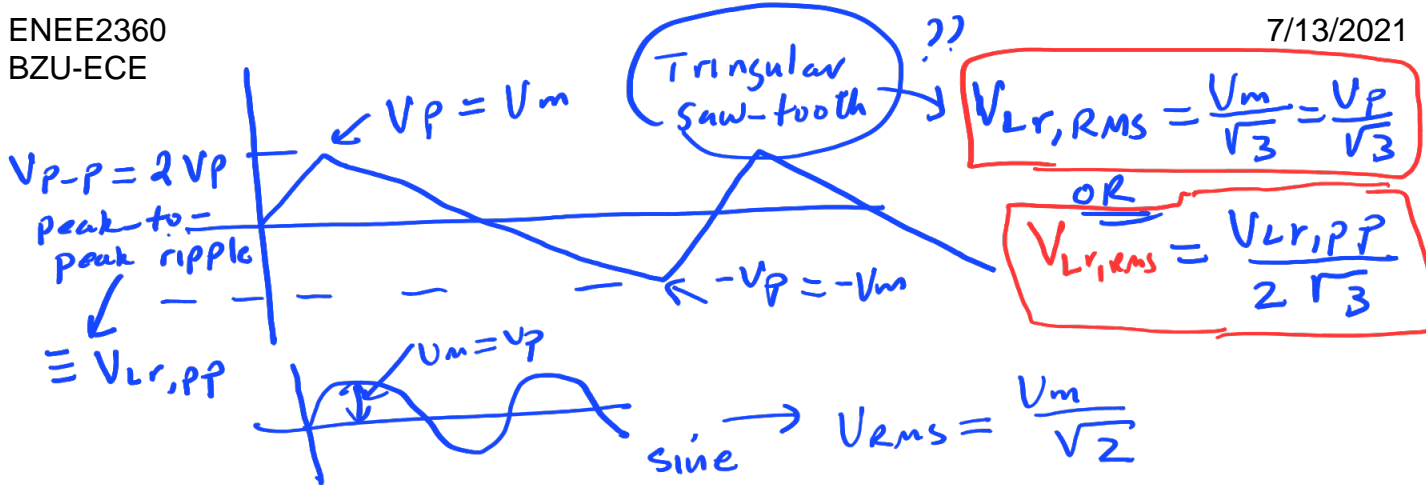
OR

$$V_{O,DC} = V_m - \frac{1}{2} V_{Lr,p-p}$$

where  $V_m = 10$   
 $V_{Lr,p-p} = 2$

$$V_{O,DC} = 10 - \frac{1}{2} \cdot 2 = 9V$$

?  $r\% = \frac{\text{RMS value}}{\text{average}} \cdot 100\%$



- Also for a triangular signal,

RMS Value =  $\frac{\text{Peak Value}}{\sqrt{3}}$  \*\*\*

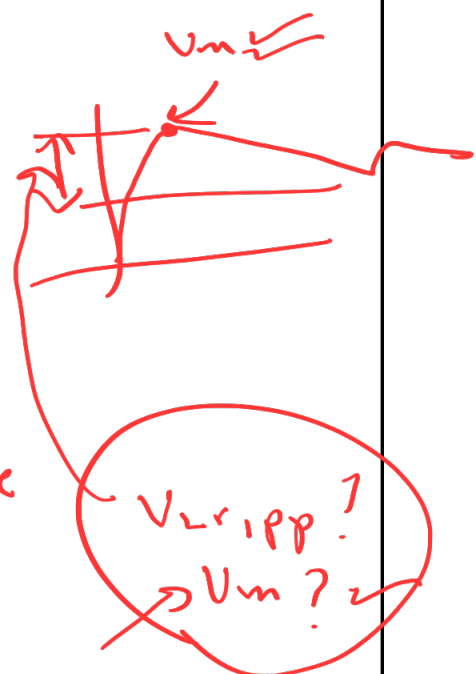
OR

RMS Value =  $\frac{\text{Peak to peak Value}}{2\sqrt{3}} = \frac{V_{Lr,p-p}}{2\sqrt{3}}$

\*\*\*  $\therefore r\% = \frac{\frac{V_{Lr,p-p}}{2\sqrt{3}}}{V_m - \frac{1}{2}V_{Lr,p-p}} \cdot 100\%$

$\rightarrow$  RMS ripple

$\rightarrow$  dc value



$\Rightarrow$  To Determine the ripple factor we need to find the peak to peak ripple  $V_{Lr,p-p}$

$\rightarrow V_m$  ?

$\rightarrow C$

$\rightarrow f$

$\rightarrow R$



$V_m = V_{max}$   
 $V_c = V_{max} e^{-\frac{t}{\tau}}$   
 $V_{min}!$  in general  $= V_{max} e^{-\frac{(t-t_0)}{\tau}}$

### Ripple Factor

For  $t_2 > t > t_1$

discharge equation

$$V_L(t) = V_m e^{-\frac{(t-t_1)}{RC}}$$

$$V_{Lr,p-p} = V_L(t_1) - V_L(t_2)$$

$$V_{Lr,p-p} = V_m - V_m e^{-\frac{(t_2-t_1)}{RC}}$$

$$V_{Lr,p-p} = V_m \left[ 1 - e^{-\frac{(t_2-t_1)}{RC}} \right]$$

using  $e^{-x} \approx 1 - x$

cap. discharge

$V_m$ ,  $V_0$ ,  $v_{Lr,pp}$

$t_1$ ,  $t_2$ ,  $t$

$V_p$ ,  $v_1$ ,  $v_0$ ,  $V_r$ ,  $\Delta r$

Conduction interval  $\Delta r$

(b)

$i_D$ ,  $i_L$

\*  $V_{Lr,pp} = V_m \left[ 1 - \left( 1 - \frac{t_2-t_1}{RC} \right) \right] = V_m \left[ \frac{t_2-t_1}{RC} \right]$  \*\*

\*  $V_{L,dc} = V_{L,avg} = V_m - \frac{1}{2} V_{Lr,pp}$

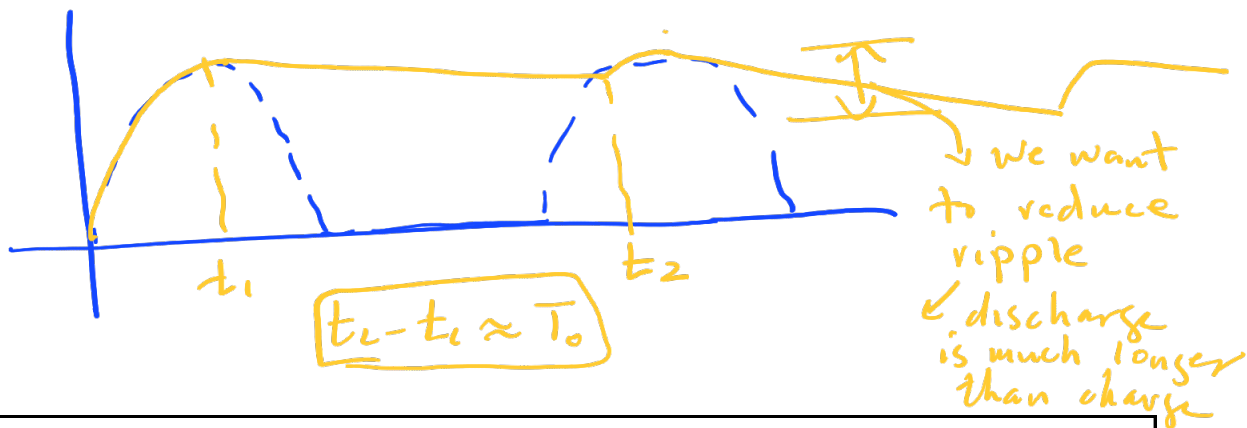
\*  $r\% = \frac{RMS \text{ ripple}}{V_{L,dc}} \cdot 100\%$

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using  $e^{-x} \cong 1 - x$

$$V_{Lr,p-p} = V_m \left[ 1 - e^{-\frac{(t_2 - t_1)}{RC}} \right] \Rightarrow V_{Lr,p-p} = V_m \left( \frac{(t_2 - t_1)}{RC} \right)$$

$$V_{L,dc} = V_m - \frac{1}{2} V_{Lr,p-p}$$



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a) For Half Wave Rectifier

$$t_2 - t_1 \cong T_0 = \frac{1}{f_0}$$

$$V_{Lr,p-p} = V_m \left( \frac{T_0}{RC} \right) = V_m \left( \frac{1}{f_0 RC} \right)$$

$$V_{L,dc} = V_m \left( 1 - \frac{1}{2f_0 RC} \right)$$

$$(V_{L,r})_{RMS} = \frac{V_{Lr,p-p}}{2\sqrt{3}}$$

$$(V_{L,r})_{RMS} = \frac{V_m}{2\sqrt{3}f_0 RC}$$

$$\therefore r \% = \frac{(V_{L,r})_{RMS}}{V_{L,dc}} 100\%$$

$$\therefore r \% = \frac{1}{\sqrt{3}[2f_0 RC - 1]} 100\%$$



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b) For Full Wave Rectifier

$$t_2 - t_1 \cong \frac{1}{2} T_o = \frac{1}{2f_o}$$

$$V_{Lr,p-p} = V_m \left( \frac{T_o}{2RC} \right) = V_m \left( \frac{1}{2f_o RC} \right)$$

$$V_{L,dc} = V_m \left( 1 - \frac{1}{4f_o RC} \right)$$

$$(V_{L,r})_{RMS} = \frac{V_{Lr,p-p}}{2\sqrt{3}}$$

$$(V_{L,r})_{RMS} = \frac{V_m}{4\sqrt{3}f_o RC}$$

Half wave

$$\rightarrow V_{ripp} = \frac{V_m}{f_o RC}$$



$$\therefore r \% = \frac{1}{\sqrt{3}[4f_o RC - 1]} 100\%$$

X

$$r\% = \frac{\text{RMS ripple}}{\text{dc value}} \cdot 100\%$$

$$V_{Lr,RMS} = \frac{V_{Lr,pp}}{2\sqrt{3}} ; \quad V_{Lr,pp} = \frac{V_m}{2f_0RC}$$

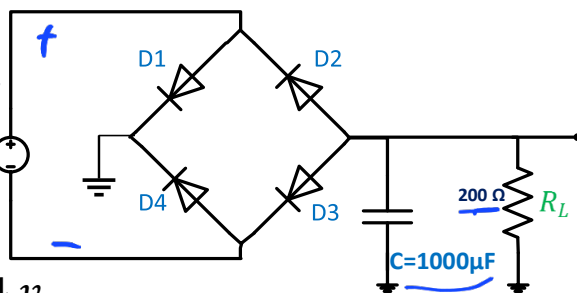
$$V_{in,p} = V_m = 30\sqrt{2}$$

### Example

Find the ripple factor  $r\%$

Input = 30V RMS

$f = 60$  Hz



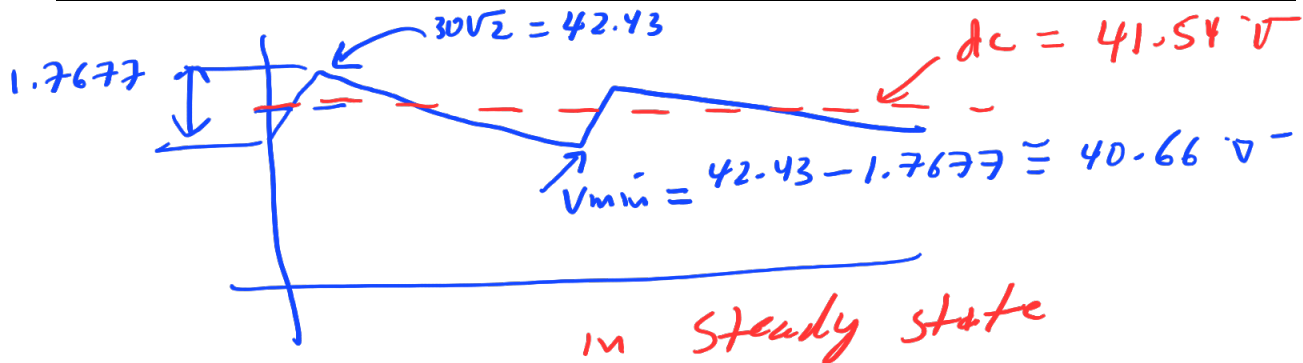
$$V_{L,dc} = V_m - \frac{1}{2} \frac{V_m}{2f_0R_{LC}} = 41.54 \text{ v}$$

$$V_{Lr,p-p} = \frac{V_m}{2f_0R_{LC}} = 1.7677 \text{ v} = \frac{30\sqrt{2}}{2 \times 60 \times 200 \times 1000 \mu\text{F}} = 1.7677$$

$$\text{RMS (ripple voltage)} = \frac{V_{Lr,p-p}}{2\sqrt{3}} = 0.51 \text{ v rms}$$

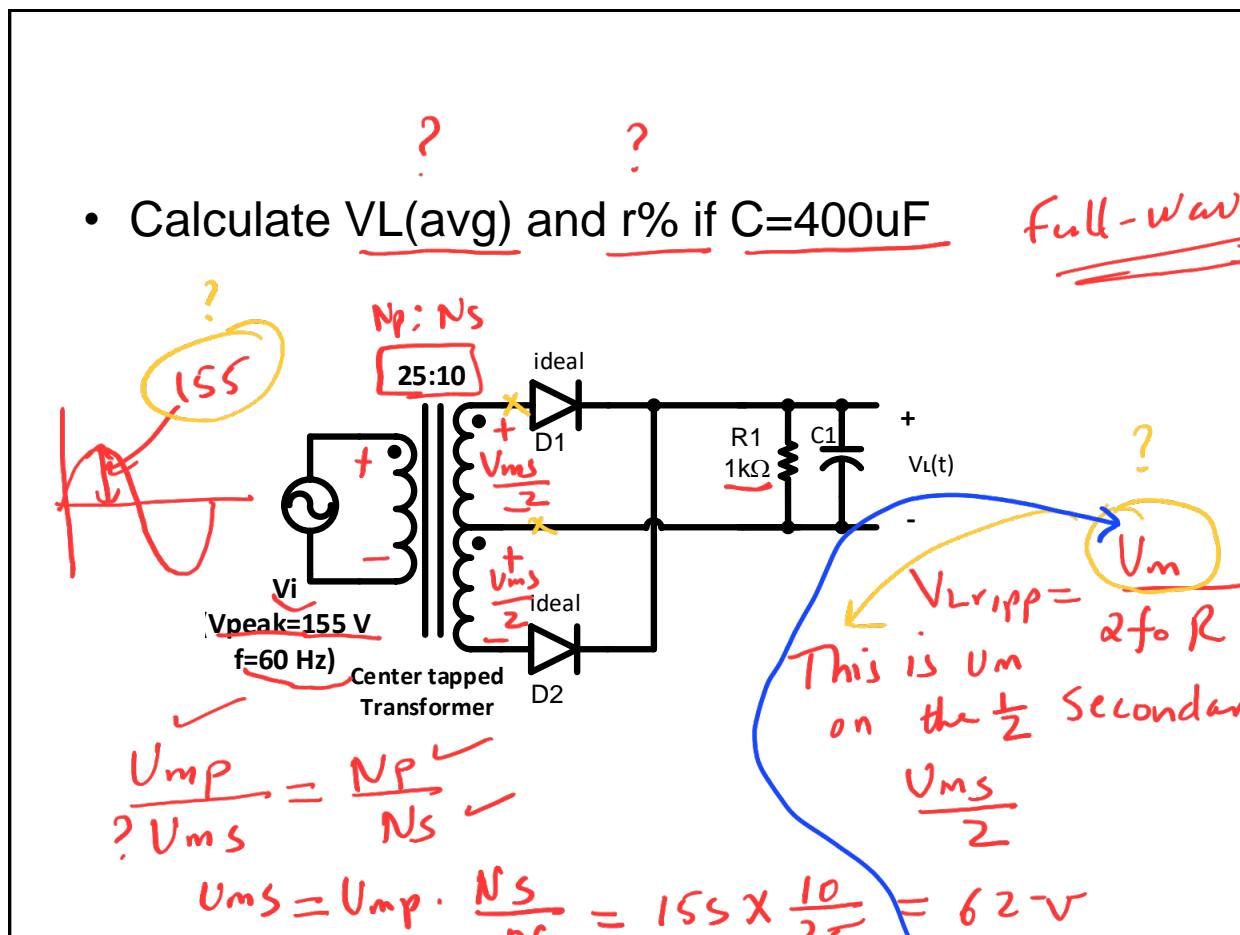
$$\therefore r = \frac{0.51}{41.54} \times 100\%$$

$$r = 1.2277\%$$



- Calculate  $V_L(\text{avg})$  and  $r\%$  if  $C=400\mu\text{F}$

Full-wave



$$\frac{U_{mp}}{? U_{ms}} = \frac{N_p}{N_s}$$

$$U_{ms} = U_{mp} \cdot \frac{N_s}{N_p} = 155 \times \frac{10}{25} = 62 \text{ V}$$

$$\frac{U_{ms}}{2} = \frac{62}{2} = 31 \text{ V}$$

$$V_{L(\text{ripple})} = \frac{31}{2 \times 60 \times 1 \text{ k} \times 400 \mu\text{F}} = 0.6458 \text{ V}$$

$$V_{L(\text{avg})} = U_m - \frac{1}{2} V_{L(\text{ripple})} = 31 - \frac{1}{2} (0.6458) = 30.677 \text{ V}$$

$$r\% = \frac{V_{L,ripple}}{2\sqrt{3} V_{L,avg}} \cdot 100\%$$

$$= \frac{0.6458}{2\sqrt{3} \cdot 30.677} \cdot 100\% = 0.607\%$$

## Home Work 1

Sample not to be solved

**NOTE THAT EACH STUDENT WILL HAVE DIFFERENT DESIGN TARGET**

- Design a rectifier with filter to provide an a load ( $R_L = 0.45 \text{ kohm}$ ) with an average voltage equal to  $20 \text{ Vdc}$  with a ripple factor  $= 4.5\%$ ,  $V_{in}$  is sinusoidal with  $220 \text{ Vrms}$ ,  $f = 50 \text{ Hz}$
- Perform the design three times using :

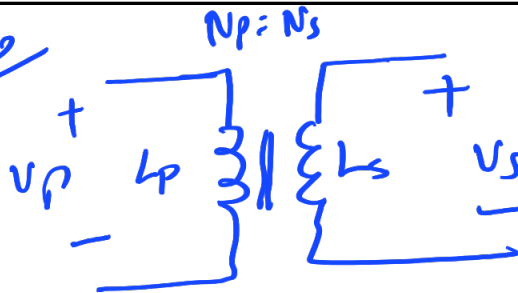
- Half Wave rectifier
- Bridge Full wave rectifier
- Center tapped full wave rectifier



Simulate your designed circuits using Pspice

+ Transfer + filter

حل المسألة



K-coupling  
K = 1

$$\frac{V_P}{V_S} = \frac{N_P}{N_S} = \sqrt{\frac{L_P}{L_S}}$$